

Event-driven Optimization-based Control of Hybrid Systems with Integral Continuous-time Dynamics

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Abstract

In this paper we introduce a class of continuous-time hybrid dynamical systems called *integral continuous-time hybrid automata* (icHA) for which we propose an event-driven optimization-based control strategy. Events include both external actions applied to the system and changes of continuous dynamics (mode switches). The icHA formalism subsumes a number of hybrid dynamical systems with practical interest, e.g., linear hybrid automata. Different cost functions, including minimum-time and minimum-effort criteria, and constraints are examined in the event-driven optimal control formulation. This is translated into a finite-dimensional mixed-integer optimization problem, in which the event instants and the corresponding values of the control input are the optimization variables. As a consequence, the proposed approach has the advantage of automatically adjusting the attention of the controller to the frequency of event occurrence in the hybrid process. A receding horizon control scheme exploiting the event-based optimal control formulation is proposed as a feedback control strategy and proved to ensure either finite-time or asymptotic convergence of the closed-loop.

Key words: Hybrid systems, discrete-event systems, optimal control, model predictive control, mixed-integer programming.

1 Introduction

Hybrid systems are capable of modelling complex processes characterized by the coexistence and interaction of discrete and continuous dynamics [1]. The hybrid dynamics are usually described either in discrete-time through difference equations, or in continuous-time through differential equations. The trajectory of a continuous-time hybrid system can be represented as a sequence of continuous evolutions interleaved by discrete events [2,3], which cause changes in the set of differential equations defining the continuous flow, also called the “modes” of the hybrid system. Such a behavior is exhibited, for instance, by piecewise affine systems, where the coefficients of the linear differential or difference equations defining the continuous dynamics depend on linear inequality conditions over the continuous state and input vectors [4].

As mode switches introduce discontinuities in the vector fields defining the system dynamics, this may lead to weaker solution concepts for the differential equations, such as the Filippov [5] or Utkin [6] solutions, and also to pathological effects, such as Zeno behaviors [3]. The presence of possible resets of the state values after mode switches further complicates the trajectory, as in this case the trajectory itself can become discontinuous. The continuous flow and the instants at which the discrete events occur can be further influenced by exogenous discrete and continuous input

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signals. From a controller design perspective, when optimal control is applied to continuous-time hybrid systems, the resulting computational problem is hard to solve, since it usually involves nonconvex problems (see [7] and the references therein).

In the discrete-time setting not only most of the aforementioned subtleties in the characterization of trajectories disappears, but also optimal control problems can be solved very efficiently through mixed-integer programming (MIP) solvers [8]. In comparison with the continuous-time case, here the simplification is mainly due to the fact that events (such as mode switches) can only occur at sampling instants. However, mode switches that occurs in the intersampling, and hence are not unrecognized or delayed, may lead to non-negligible modelling errors [9, Ch. 5] that we call mode-mismatch. In the discrete-time case, modelling precision can be improved by reducing the sampling period. However, this increases the computational load of the controller. In particular, in a model predictive control (MPC) context [10], the obvious disadvantage is that, for a given time-horizon of prediction, a larger number of control variables is involved in the optimization problem.

To avoid mode-mismatch errors one should change command values exactly when the mode changes, or in other words adopt an *event-driven* control approach. Event-driven approaches have been originally used for control in the framework of discrete-event systems, e.g., finite state machines and Petri nets. Receding horizon control approaches have been successfully applied to some classes of discrete-event systems, max-plus-linear discrete event systems [11], discrete-event systems with real-time constraints [12], and scheduling systems [13].

This paper introduces *integral continuous-time hybrid automata* (icHA), a model paradigm for a special class of continuous-time hybrid dynamical systems for which no a priori information about the timing and order of the events is assumed. It will be shown that the dynamics of an icHA can be expressed with an event-driven formulation, as will be detailed in Section 2. A similar formulation has been used in plant [14]. In Section 3 we formulate different continuous-time optimal control problems of icHA that can be solved via mixed integer programming techniques despite the event-driven formulation. A similar approach was proposed in [15], although the system model and the optimization approach are different: in [15] mode switches are directly controlled and the system dynamics have no other exogenous input signals, that also induces a solution algorithm based on linear programming and enumeration of feasible mode sequences. Finally, the optimal control methods are used in Section 4 to develop an event-driven closed-loop control approach that exploits a model predictive control philosophy, for which conditions for convergence are given together with an illustrative example.

1.1 Notation

Small letters denote variables or vectors (e.g., v , ξ), superscripts (e.g., v^j) vector components. Subscripts are used for system modes (e.g., A_i , b_i , f_i) and for time instants in a sequence of time instants (t_i). Bold symbols denote finite sequences of variables, e.g., $\mathbf{a} \triangleq \{a(t_i)\}_{i=0}^N$. The sets \mathbb{R} and \mathbb{Z} indicate the set of real numbers and integer numbers, respectively, \mathbb{Z}_{0+} , \mathbb{R}_{0+} , \mathbb{Z}_{0+} , \mathbb{R}_{+} indicate the sets of nonnegative integer, nonnegative real, positive integer, and positive real numbers, respectively. We use $\mathbb{Z}_{[a,b]}$ where $a, b \in \mathbb{Z}$, $b \geq a$ to indicate the set $\{x \in \mathbb{Z} : a \leq x \leq b\}$. We indicate the origin of a space by \mathcal{O} , the interior of a set \mathcal{X} by $\text{Int}(\mathcal{X})$ and its closure by $\text{Cl}(\mathcal{X})$. The binary operator \setminus indicates the difference between sets.

Relational operators (such as \leq) over vectors are intended componentwise. For matrices, $Q \geq 0$ indicates positive semidefiniteness, $\|z\|_\infty^Q \triangleq \max_i |(Qz)^i|$, $\|z\|_1^Q \triangleq \sum_i |(Qz)^i|$, and $\|z\|_2^Q \triangleq z^T Q z$ where $Q > 0$. The symbol I indicates the identity matrix of appropriate dimensions, while we use the bold $\mathbf{0}$ and $\mathbf{1}$ to indicate matrices and vectors entirely composed of zeros and ones, respectively. The symbol \rightarrow denotes logical implication (*if*) and the symbol \leftrightarrow logical equivalence (*iff*).

Given a signal $a(\cdot) : \mathbb{R}_{0+} \rightarrow \mathbb{A}$ we indicate its continuous-time trajectory by $a(s)$, $s \in \mathbb{R}_{0+}$, and its event-driven trajectory by $a(j)$, where $j \in \mathbb{Z}_{0+}$, $a(j) = a(t_j)$ and t_j is the time instant at which the j^{th} event occurs. When considering event-driven predictive control, the predicted trajectory of a signal $a(\cdot)$ from state $x(t)$ at time t along event steps $\mathbb{Z}_{[r,s]}$ are indicated by $\mathbf{a}(x(t)) = [a_{x(t)}(r), \dots, a_{x(t)}(s)]$.

2 Integral Continuous-time Hybrid Automaton

We consider a continuous-time version of the discrete hybrid automaton (DHA) proposed in [16], denoted as *integral continuous (-time) hybrid automaton* (icHA), where discrete-time affine dynamics are replaced by integral continuous-time dynamics. Similarly to DHA, the icHA consists of the four components reported in Figure 1: the integral switched

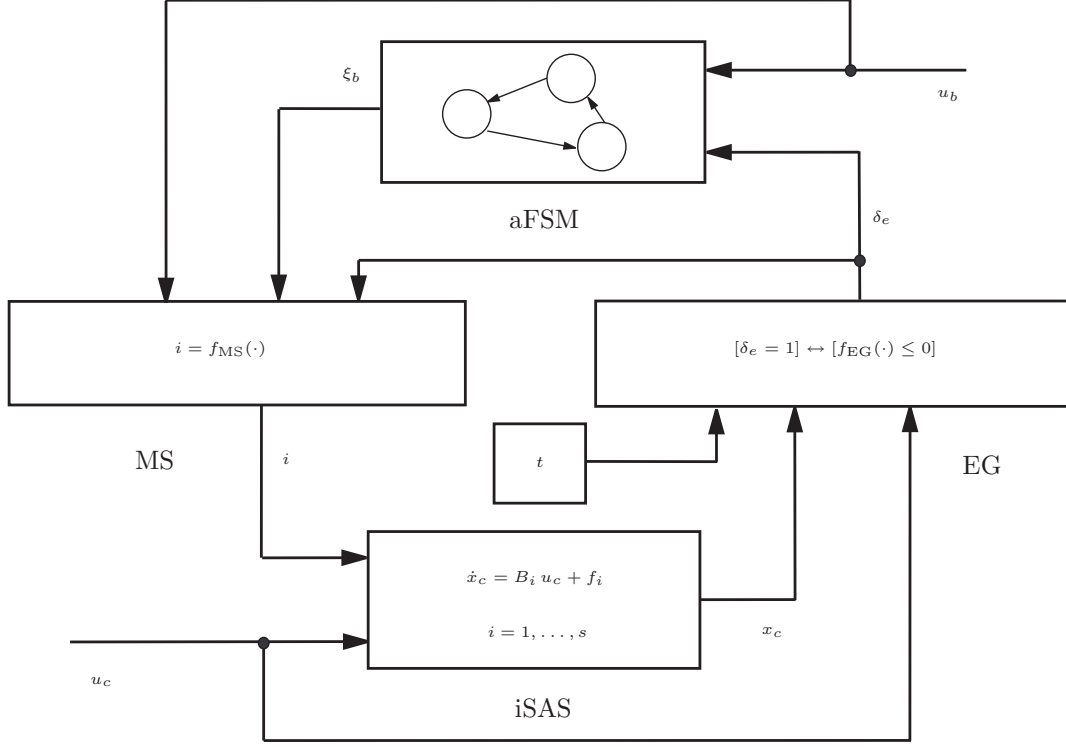


Fig. 1. Integral Continuous-time Hybrid Automaton (icHA).

affine system (iSAS), the event generator (EG), the mode selector (MS) and the asynchronous finite state machine (aFSM). The iSAS represents a collection of continuous-time integral dynamics for the continuous states

$$\dot{x}_c(t) = B_{i(t)}u_c(t) + f_{i(t)}, \quad (1)$$

where $x_c \in \mathbb{R}^{n_c}$ and $u_c \in \mathbb{R}^{m_c}$ are the continuous components of the state and input vectors, respectively, and $i \in \mathcal{I} = \{1, 2, \dots, s\}$ is the system mode. As will be detailed later, the main reason for restricting the attention on integral dynamics instead of more general linear dynamics is computational. Nonetheless, the class of continuous-state dynamics (1) has been widely exploited for modelling and verification of hybrid systems [2, 15, 17], as it is powerful enough to model many practical problems. In fact, given a nonlinear (possibly discontinuous) dynamical model $\dot{x}_c = f(x_c(t), u_c(t))$, model (1) can be interpreted as a piecewise zero-order approximation of the state-transition function with respect to the state vector x_c and a first-order approximation with respect to the input vector u_c . Similarly to the piecewise affine (PWA) approximation $\dot{x}_c = A_i x_c + B_i u_c + f_i$, the icHA dynamics can be arbitrarily close to a given nonlinear dynamics by augmenting the number of modes.

The EG defines the *endogenous* binary inputs δ_e according to the linear threshold conditions

$$[\delta_{e_x}^i(t) = 1] \leftrightarrow [E_i^x \begin{bmatrix} x_c(t) \\ t \end{bmatrix} \leq F_i^x], \quad i \in \mathbb{Z}_{[1, n_e^x]}, \quad (2a)$$

$$[\delta_{e_u}^i(t) = 1] \leftrightarrow [E_i^u u_c(t) \leq F_i^u], \quad i \in \mathbb{Z}_{[1, n_e^u]}, \quad (2b)$$

and we get $\delta_e \triangleq [\delta_{e_x}^1 \dots \delta_{e_x}^{n_e^x} \delta_{e_u}^1 \dots \delta_{e_u}^{n_e^u}]^T \in \{0, 1\}^{n_e}$, $n_e \triangleq n_e^x + n_e^u$, as the vector of endogenous binary input variables. The icHA may be also excited by *exogenous* binary input signals $u_b \in \{0, 1\}^{m_b}$ entering the mode selector and the asynchronous finite state machine described below.

Definition 2.1 $\mathcal{PC}_{(m_c, m_b)}$ is the set of piecewise constant functions $u(t) \triangleq \begin{bmatrix} u_c(t) \\ u_b(t) \end{bmatrix}$, $u : \mathbb{R} \rightarrow \mathbb{R}^{m_c} \times \{0, 1\}^{m_b}$ such that $u(t)$ is constant for all $t \in [t_k, t_{k+1})$, $k \in \mathbb{Z}_{0+}$, where $t_0 < t_1 < \dots$ is a sequence of time instants. \square

Discrete-time samples held constant between sampling instants by a zero-order holder are a special case of piecewise constant functions, corresponding to equally spaced time instants. General piecewise constant functions can approximate arbitrarily well any given piecewise continuous function, provided that the number of intervals can go to infinity and the interval length can go to 0.

Assumption 2.1 *In what follows it is assumed that $u : \mathbb{R} \rightarrow \mathbb{R}^{m_c} \times \{0, 1\}^{m_b} \in \mathcal{PC}_{(m_c, m_b)}^1$, i.e., the input trajectory is piecewise constant along time.* \square

Definition 2.2 *An event occurs whenever an endogenous input δ_e or an exogenous input $[u_b]$ changes value. Given the initial time $t_0 \in \mathbb{R}$, the event instants are defined recursively as*

$$t_k \triangleq \min_{t > t_{k-1}} \{t : (u_c(t), u_b(t), \delta_e(t)) \neq (u_c(t_{k-1}), u_b(t_{k-1}), \delta_e(t_{k-1}))\}, \quad (3)$$

where clearly $t_j < t_{j+1}$ for all $j \in \mathbb{Z}_{0+}$. We assume that the minimum in (3) always exists. \square

The Boolean state $\xi_b \in \{0, 1\}^{n_b}$ is defined as

$$\begin{aligned} \xi_b(t) &\triangleq x_b(t_k) \text{ for } t_{k-1} \leq t < t_k, \\ x_b(t_{k+1}) &= f_{\text{aFSM}}(x_b(t_k), u_b(t_k), \delta_e(t_k)), \end{aligned} \quad (4) \quad (5)$$

and $f_{\text{aFSM}} : \{0, 1\}^{n_b+m_b+n_e} \rightarrow \{0, 1\}^{n_b}$ is the Boolean function defining the transitions of the asynchronous finite state machine. The Boolean state $\xi_b(t)$ remains constant, $\xi_b(t) = x_b(t_k)$, during the whole interval $t_{k-1} \leq t < t_k$. At the event instant t_k , the Boolean state switches to the new value $f_{\text{aFSM}}(x_b(t_k), \delta_e(t_k), u_b(t_k))$, and remains at that value for $t_k \leq t < t_{k+1}$. While we are assuming that the transitions of the aFSM are instantaneous, delays can be easily modelled by introducing additional events and states. In (5) discrete-state transitions can occur at any time instant, not only at multiples of a given sampling period as for DHA.

The different operating modes of the system represented by the variable $i(t)$ are selected by the mode selector (MS) function through the scalar product

$$i(t) = [1 \ 2 \ \dots \ s] \cdot f_{\text{MS}}(\xi_b(t), u_b(t), \delta_e(t)), \quad (6)$$

where $f_{\text{MS}} : \{0, 1\}^{n_b+m_b+n_e} \rightarrow \{0, 1\}^s$ is a Boolean function satisfying the mutual exclusivity relation $\mathbf{1}^T \cdot f_{\text{MS}}(\xi_b(t), u_b(t), \delta_e(t)) = 1$, for all $(\xi_b(t), u_b(t), \delta_e(t)) \in \{0, 1\}^{n_b+m_b+n_e}$. In (6), when u_b and δ_e remain constant the Boolean state and the system mode also remain constant.

2.1 Event-Driven Representation of icHA

The icHA model (1)–(6) is next converted to a computationally-oriented event-driven representation.

Let $\mathbf{t} = \{t_j\}_{j=0}^{h-1}$ be a finite sequence of ordered time instants $t_0 < t_1 < \dots < t_{h-1}$. Let $u_c : \mathbb{R} \rightarrow \mathbb{R}^{m_c}$ be a piecewise constant function with breakpoints at the instants in \mathbf{t} and $\mathbf{u} = \{u_c(t_k)\}_{k=0}^{h-1}$ the corresponding sequence of levels. For the affine dynamics $\dot{x}_c(t) = Ax_c(t) + Bu(t) + f$, the state value at t_j , $j \in \mathbb{Z}_{[0, h-1]}$, is a nonlinear function of \mathbf{t} and \mathbf{u} . However in the case of integral dynamics ($A = \mathbf{0}$),

$$x_c(t_j) = x_c(t_0) + \sum_{k=0}^{j-1} (B(t_{k+1} - t_k)u_c(t_k) + (t_{k+1} - t_k)f(t_k)). \quad (7)$$

Consider now a system with switched integral dynamics (1), and let the set of mode-switch instants $\{t : i(t - \varepsilon) \neq i(t + \varepsilon), \varepsilon \rightarrow 0\} \subseteq \mathbf{t}$. Since in any time interval $[t_k, t_{k+1})$ the mode is constant, from (7) we obtain that the system

¹ For the simplicity of notation the subscript (m_c, m_b) will be dropped in the rest of the paper when the value of m_c and m_b is clear from the context.

dynamics can be rewritten as the first order linear difference equations

$$x_c(k+1) = x_c(k) + B_{i(k)}v_c(k) + f_{i(k)}q(k) \quad (8a)$$

$$t(k+1) = t(k) + q(k) \quad (8b)$$

where k is the event counter, $x_c(k) = x_c(t_k)$, $t(k) = t_k$, $i(k) = i(t_k)$, $q(k)$ is the time interval between event instants t_k and t_{k+1} , $v_c(k) = q(k)u_c(k)$ is the integral over time period $q(k)$ of the input $u_c(k) = u_c(t_k)$. Note that in (8b) time t is treated as an additional state variable. The controlled variables are the input integral $v_c(k)$ and the input level duration $q(k)$, from which the actual input $u_c(k) = \frac{v_c(k)}{q(k)}$ to be applied to the continuous-time system is immediately recovered.

The event generator becomes

$$[\delta_{e_x}^i(k) = 1] \leftrightarrow \left[E_i^x \begin{bmatrix} x_c(k) \\ t(k) \end{bmatrix} \leq F_i^x \right], \quad i \in \mathbb{Z}_{[1, n_e^x]} \quad (9a)$$

$$[\delta_{e_u}^i(k) = 1] \leftrightarrow [E_i^u v_c(k) \leq F_i^u q(k)], \quad i \in \mathbb{Z}_{[1, n_e^u]}, \quad (9b)$$

where $\delta_e(k) = \delta_e(t_k)$, and $\delta_e(t) = \delta_e(t_k)$, for all $t \in [t_k, t_{k+1})$ by the definition of t_k in (3). The dependence on time becomes a dependence on a state variable, because of (8b), and (9b) is obtained from (2b) by multiplying by $q(k)$ both sides of the right clause. The mode selector equation becomes

$$i(k) = [1 \ 2 \ \dots \ s] \cdot \tilde{f}_{\text{MS}}(x_b(k), u_b(k), \delta_e(k)), \quad (10)$$

where $i(t) = i(k)$, for all $t \in [t_k, t_{k+1})$, as a consequence of the event definition, and $\tilde{f}_{\text{MS}}(x_b(k), u_b(k), \delta_e(k)) = f_{\text{MS}}(f_{\text{aFSM}}(x_b(k), u_b(k), \delta_e(k)), u_b(k), \delta_e(k))$ because of (6) and of the definition of $\xi_b(t)$. Finally, Equation (5) is already defined with respect to the events instants.

Equations (5), (8), (9), (10) define the behavior of the icHA in an event-driven representation. However, to account for (3), the following condition must be ensured:

$$[(\delta_e(k), u_c(k), u_b(k)) = (\bar{\delta}_e, \bar{u}_c, \bar{u}_b)] \rightarrow [(\delta_e(t), u_c(t), u_b(t)) = (\bar{\delta}_e, \bar{u}_c, \bar{u}_b), \quad \forall t \in [t_k, t_{k+1})]. \quad (11)$$

We consider two different cases: (i) the value u_c or u_b changes, so that an event is externally forced, for instance by a controller, (ii) the value of δ_e changes, i.e., an endogenous event occurs. Since we will focus on an event-driven control design, in which exogenous events are generated on purpose by the controller, we can assume that $u_c(t)$, $u_b(t)$ are constant between event instants and simply restrict condition (11) to

$$[\delta_e(k) = \bar{\delta}_e] \rightarrow [\delta_e(t) = \bar{\delta}_e, \quad \forall t \in [t_k, t_{k+1})], \quad (12)$$

i.e., that the current mode is kept until the next event. Moreover, as $\delta_{e_u}^i$ variables in (2b) can change only when the input changes, they can be dealt with as for externally forced events, namely by appropriate selection of the control inputs. Thus, it is indeed sufficient to enforce (12) for the variables in (2a).

Let the mapping $\text{cod}(\cdot) : \{0, 1\}^{n_e} \rightarrow \mathbb{Z}_{0+}$ associate a nonnegative integer number d to each allowed value of vector $\delta_e^x = [\delta_{e_x}^1 \dots \delta_{e_x}^{n_e^x}]^T$ defined in (2a). For example d may be the integer whose binary encoding is δ_{e_x} . Define the matrix $\bar{E}^x(d)$ and the vector $\bar{F}^x(d)$ by collecting the rows in the inequalities of the EG (9) which are satisfied for e^x such that $\text{cod}(\delta_{e_x}) = d$. Define $\hat{E}^x(d)$, $\hat{F}^x(d)$ by collecting as rows the inequalities of the EG (9), which are not satisfied for δ_{e_x} such that $\text{cod}(\delta_{e_x}) = d$. Hence (12) is equivalently replaced by

$$[\text{cod}(\delta_{e_x}(k)) = d] \rightarrow [\bar{E}^x(d) \begin{bmatrix} x \\ t \end{bmatrix} \leq \bar{F}^x(d), \quad \hat{E}^x(d) \begin{bmatrix} x \\ t \end{bmatrix} > \hat{F}^x(d)], \quad \forall t \in [t_k, t_{k+1}). \quad (13)$$

As an example, consider two thresholds $[\delta_{e_x}^1 = 1] \leftrightarrow [x \leq 0]$, $[\delta_{e_x}^2 = 1] \leftrightarrow [x \leq 1]$. The matrices associated to $\delta_{e_x}^x = [0 \ 1]^T$, where $\text{cod}(\delta_{e_x}) = 1$, are $\bar{E}^x(1) = 1$, $\bar{F}^x(1) = 1$, collecting the second threshold condition (satisfied), and $\hat{E}^x(1) = 1$, $\hat{F}^x(1) = 0$.

Proposition 2.1 Let $\text{cod}(\tilde{\delta}_{e_x}) = d$, and let $\bar{E}^x(d)$, $\hat{E}^x(d)$ and $\bar{F}^x(d)$, $\hat{F}^x(d)$ be the associated matrices and vectors, respectively, obtained by collecting the rows in (9) which are either satisfied (\bar{E}^x , \bar{F}^x) or not satisfied (\hat{E}^x , \hat{F}^x) when δ_{e_x} is such that $\text{cod}(\delta_{e_x}) = d$. In case of integral dynamics, if $u_c(t)$ is constant for $t \in [t_k, t_{k+1})$, (12) is guaranteed by the mixed-logical constraint

$$\left[\text{cod}(\delta_e^x(k)) = d \right] \rightarrow \left[\begin{bmatrix} \bar{E}^x(d) \\ -\hat{E}^x(d) \end{bmatrix} \begin{bmatrix} x(k+1) \\ t(k+1) \end{bmatrix} \leq \begin{bmatrix} \bar{F}^x(d) \\ -\hat{F}^x(d) \end{bmatrix} + \varepsilon \mathbf{1} \right], \quad (14)$$

for $\varepsilon > 0$, $\varepsilon \rightarrow 0^+$.

Proof. Because of the integral dynamics, the state trajectory for $t \in [t_k, t_{k+1})$ is the line $x(t) = x(k) + \gamma(t - t(k))$, where $\gamma = \frac{x(k+1) - x(k)}{t(k+1) - t(k)}$. Condition (13) and condition (14) define two polyhedra, \mathcal{P} and \mathcal{P}_ε , respectively. Since $\varepsilon > 0$, $\mathcal{P}_\varepsilon \supset \mathcal{P}$ and if $\varepsilon \rightarrow 0$, $\mathcal{P}_\varepsilon \rightarrow \mathcal{P}$. Condition (14) ensures that $x(k+1) \in \mathcal{P}_\varepsilon$ and (13) ensures that $x(k) \in \mathcal{P} \subset \mathcal{P}_\varepsilon$, hence for all $t \in [t_k, t_{k+1}]$, $x(t) \in \mathcal{P}_\varepsilon$. Thus, by linearity of the trajectory there exists $\varrho(\varepsilon)$ such that $x(t) \in \mathcal{P}$, for all $t \in [t_k, t_{k+1} - \varrho(\varepsilon)]$. Since for $\varepsilon \rightarrow 0$, $\mathcal{P}_\varepsilon \rightarrow \mathcal{P}$, then for $\varepsilon \rightarrow 0$ also $\varrho(\varepsilon) \rightarrow 0$. \square

The effect of adding ε in equation (14) is to expand the polyhedron \mathcal{P} . This is necessary for allowing $\delta_e^x(k+1) \neq \delta_e^x(k)$, otherwise the system would be constrained to remain always in the same mode. The value of $\varrho(\varepsilon)$ is the time the trajectory spends in $\mathcal{P}_\varepsilon \setminus \mathcal{P}$. When $\mathcal{P}_\varepsilon \rightarrow \mathcal{P}$, $\varrho(\varepsilon) \rightarrow 0$.

Note that, within a given mode $i(k)$, $x(k+1)$ is an affine function of $x(k)$, $q(k)$, and $v(k) \triangleq \begin{bmatrix} v_c(k) \\ v_b(k) \end{bmatrix}$, where $v_b(k) = u_b(k)$, so that (14) can be reformulated as a set of mixed-integer inequalities on $x(k)$, $q(k)$, $v(k)$, $\delta_e(k)$ [18]. Indeed, equations (5), (8), (9), (10), (14) represent a DHA that can be converted into the *event-driven MLD* (eMLD) system

$$x(k+1) = Ax(k) + B_1w(k) + B_2\delta_e(k) + B_3z(k) + B_5, \quad (15a)$$

$$t(k+1) = t(k) + q(k), \quad (15b)$$

$$E_2\delta_e(k) + E_3z(k) \leq E_1w(k) + E_4x(k) + E_5 + E_6t(k), \quad (15c)$$

where $w(k) \triangleq \begin{bmatrix} v(k) \\ q(k) \end{bmatrix}$, for instance using the tool HYSDEL [16]. Differently from the standard discrete-time MLD system [8], in the eMLD (15) k is an event counter, while time t is an additional state variable.

Remark 2.1 *Discontinuities of the continuous state trajectory in the form of state resets $x_c(t_{k+1}) = \Phi_i x_c(t_k) + \mu_i$ can be included as follows. To model resets one must add reset modes $i \in \{s+1, \dots, s_r\}$, modify (8a) into $x_c(k+1) = (\Phi_i x_c(k) + \mu_i) + B_i v(k) + f_i q(k)$, and (8b) into $t(k+1) = t(k) + \Gamma_i q(k)$, where in modes $i = \{1, \dots, s\}$, $\Phi_i = I$, $\mu_i = \mathbf{0}$, and $\Gamma_i = 1$, while in reset modes $i = \{s+1, \dots, s_r\}$ $B_i = \mathbf{0}$, $f_i = \mathbf{0}$, and $\Gamma_i = \mathbf{0}$.*

When a reset occurs Equation (12) does not apply, as $t_{k+1} = t_k$. In this case, assuming that two consecutive resets cannot occur, the continuous-time trajectory $x_c(t)$ may be discontinuous in t_k , and is defined as follows. Let j , be the mode immediately before the reset mode i . Then, $\lim_{t \rightarrow t_k^-} x_c(t) = x_c(k-1) + B_j v(k-1) + f_j q(k-1)$, $x_c(t_k) = \Phi_i(x_c(k-1) + B_j v(k-1) + f_j q(k-1)) + \mu_i$, and $\lim_{t \rightarrow t_k^+} x_c(t) = x_c(t_k)$. In other words, we define the state trajectory $x_c(t)$ as right continuous.

In accordance with the above definition of resets, in eMLD models these are instantaneous, contrary to resets in discrete-time MLD models that are constrained to last one sampling interval [16]. An equivalent event-driven PWA system (ePWA) of the eMLD (15) can be obtained [19]. See [9] for further details.

2.2 Modelling Capabilities

Even though the piecewise integral dynamics of the continuous-state of icHA has some limitations, the icHA cover several popular model classes.

Linear hybrid automata (LHA), known to be useful for both control [20] and verification purposes [17], can be modeled by icHA, as intuitively shown by the example in Section (3.3). A formal proof of the capabilities of icHA to model linear hybrid automata can be obtained by resorting to an equivalent piecewise affine representation of the

icHA system [9] and by exploiting the results in [21] on the relations between linear hybrid automata and piecewise affine systems. In [22] an example of formal verification of a LHA performed through its equivalent icHA formulation was given.

Another class of systems that can be modelled as icHA is the class of continuous Petri nets (CPN) [23], that relaxes classical Petri nets allowing continuous values for transition firings, to alleviate combinatorial state explosion. The dynamics of a timed continuous Petri net under finite server semantics is piecewise integral, hence the class of continuous Petri nets is contained in the class of icHA. The application to continuous Petri net control of the techniques proposed here has been presented in [24].

Finally as mentioned in Section 2, piecewise integral dynamics can approximate nonlinear dynamics arbitrarily well, possibly at the price of increasing the number of system modes, similarly to what described in [4] for piecewise affine systems.

3 Event-Driven Optimal Control

Consider the *event-driven optimal control problem* for the icHA (1)–(6)

$$\min_{\mathbf{x}, \mathbf{t}, \mathbf{q}, \mathbf{v}} J(\mathbf{x}, \mathbf{t}, \mathbf{q}, \mathbf{v}) \quad (16a)$$

$$\text{s.t. icHA dynamics (1)–(6)} \quad (16b)$$

$$g(x(k), t(k), q(k), v(k)) \leq \mathbf{0}, \quad k \in \mathbb{Z}_{[0, N-1]} \quad (16c)$$

$$g_N(x(N), t(N)) \leq \mathbf{0} \quad (16d)$$

$$x(0) = x_0, \quad t(0) = t_0, \quad (16e)$$

where $J(\cdot)$ is a convex function of $(\mathbf{x}, \mathbf{t}, \mathbf{q}, \mathbf{v})$, $\mathbf{t} = \{t(k)\}_{k=0}^N$ are the time instants at which events occur, $\mathbf{x} = \{x(k)\}_{k=0}^N$ are the corresponding state values, $\mathbf{q} = \{q(k)\}_{k=0}^{N-1}$ are the durations of the time intervals between two consecutive events, $q(k) = t(k+1) - t(k)$, $\mathbf{v} = \{v(k)\}_{k=0}^{N-1}$ are the input integrals computed on the corresponding intervals $\{[t(k), t(k+1))\}_{k=0}^{N-1}$, x_0 is a given initial state, and t_0 a given initial time. Constraints (16c), (16d) represent possible additional constraints in the optimal control problem and N is the event-based optimal control horizon, i.e., the number of events considered in the optimal control formulation.

By formulating the icHA dynamics (16b) as the equivalent eMLD model (15), problem (16) can be solved by mixed integer programming (MIP) for different objective functions (16a) and constraints (16c), (16d) as detailed in Section 3.1. The cost function and the constraints determine the type of problem to be solved. As described below, all such problems are formulated in a way that results in mixed integer linear or quadratic programming (MILP, MIQP) problems, for which efficient and reliable solvers exist.

3.1 Cost Function

Similar to the discrete-time case, the cost function in (16a) can be defined as

$$J(\mathbf{x}, \mathbf{t}, \mathbf{q}, \mathbf{v}) \triangleq F(x(N), t(N)) + \sum_{k=0}^{N-1} L(x(k), t(k), q(k), v(k)). \quad (17)$$

For instance, one can set

$$L(x, t, v, q) \triangleq \|x - \hat{x}\|_p^{Q_1} + \|t - \hat{t}\|_p^{Q_2} + \|v - \hat{v}\|_p^{R_1} + \|q - \hat{q}\|_p^{R_2} \quad (18a)$$

$$F(x, t) \triangleq \|x - \hat{x}\|_p^{Q_N} + \|t - \hat{t}\|_p^{Q_T}, \quad p \in \{1, 2, \infty\}, \quad (18b)$$

where “ $\hat{\cdot}$ ” denotes a given reference value for the corresponding vector. From the general formulation (16) we can derive specific forms of the cost function (16a) and the associated constraints (16c), (16d).

It may be required that the system state reaches a desired target state \hat{x} after N events, $x(N) = \hat{x}$, or, in a softened form, that it gets very close to it by setting $F(x(N), t(N)) = \rho \|x(N) - \hat{x}\|_\infty$, where $\rho \in \mathbb{R}_+$ is a large weight. In

alternative, one can consider a convex desired target set \mathcal{X}_N and impose the constraint $x(N) \in \mathcal{X}_N$. A target time \hat{t} or set \mathcal{T}_N can be formulated similarly.

The minimum-time criterion looks for the sequence $(\mathbf{x}, \mathbf{t}, \mathbf{q}, \mathbf{v})$ that minimizes the time needed to bring the system from x_0 to the final state \hat{x} . This can be obtained by setting

$$L(x(k), t(k), q(k), v(k)) = |q(k)| = q(k), \quad F(x(N), t(N)) = 0 \quad (19)$$

in (17).

The minimum-effort criterion looks for minimizing the intensity of the command input $u(t)$. If the ℓ_1 -norm of the input function is used, we obtain $J(\mathbf{x}, \mathbf{t}, \mathbf{q}, \mathbf{v}) = \int_0^{t_N} \|u(t)\| dt = \sum_{k=0}^{N-1} \int_{t(k)}^{t(k+1)} \|u(t)\|_1 dt$. Since u is constant in each period $[t(k), t(k+1))$, it is enough to set

$$L(x(k), t(k), q(k), v(k)) = \|v(k)\|_1, \quad F(x(N), t(N)) = 0 \quad (20)$$

in (17).

The minimum-displacement criterion looks for the trajectory that minimizes the largest deviation from a desired continuous state trajectory $\hat{x}_c(\cdot)$, that we assume piecewise linear and continuous (a special case is $\hat{x}_c(\cdot) \equiv \hat{x}$):

$$J(\mathbf{x}, \mathbf{t}, \mathbf{q}, \mathbf{v}) = \max_{t \in [t(0), t(N)]} \|x_c(t) - \hat{x}_c(t)\|_\infty. \quad (21)$$

Proposition 3.1 *Let $x_c(t)$, $\forall t \in [t_0, t_N]$, be the trajectory of continuous states of an icHA system with no resets, $t_0 < t_1 < \dots < t_N$ be the event instants, assume that $\hat{x}_c(t)$ is linear over each $[t_i, t_{i+1})$, $i = 0, \dots, N-1$ and continuous over $[t_0, t_N]$. Then*

$$\max_{t \in [t_0, t_N]} \|x_c(t) - \hat{x}_c(t)\|_\infty = \max_{k=0, \dots, N-1} \{\|x_c(t(k)) - \hat{x}_c(t(k))\|_\infty\}.$$

Proof. In the absence of resets, state trajectories of icHA are continuous, so $\|x_c(\cdot) - \hat{x}_c(\cdot)\|_\infty$ is continuous, being the composition of continuous functions ($\|\cdot\|_\infty$, $x_c(\cdot)$, $\hat{x}_c(\cdot)$), and therefore the maximum over $[t_0, t_N]$ is well defined. Moreover, function $\|x_c(\cdot) - \hat{x}_c(\cdot)\|_\infty$ is a convex function of time t on $[t(k), t(k+1)]$, being the composition of a convex function (the infinity norm) with linear functions (the state trajectory of the icHA and \hat{x}_c between two consecutive switches), and thus it attains its maximum either at $t(k)$ or at $t(k+1)$. Hence,

$$\begin{aligned} \max_{t \in [t(0), t(N)]} \|x_c(t) - \hat{x}_c(t)\|_\infty &= \max_{0 \leq k \leq N-1} \left\{ \max_{t \in [t(k), t(k+1)]} \|x_c(t) - \hat{x}_c(t)\|_\infty \right\} \\ &= \max_{0 \leq k \leq N-1} \{\max\{\|x_c(t(k)) - \hat{x}_c(t(k))\|_\infty, \|x_c(t(k+1)) - \hat{x}_c(t(k+1))\|_\infty\}\} \\ &= \max_{0 \leq k \leq N} \{\|x_c(t(k)) - \hat{x}_c(t(k))\|_\infty\}. \end{aligned} \quad (22)$$

□

Note that while (21) is not in the form (17), its equivalent form (22) still leads to a mixed-integer linear formulation of the optimal control problem.

3.2 Operating Constraints

The constraints in (16c), (16d) can involve quite general mixed-integer linear constraints on states, event instants, and inputs. By using convexity arguments and continuity of $x_c(\cdot)$ similar to the ones used in the proof of Proposition 3.1, state constraints $\underline{h} \leq Hx(t) \leq \bar{h}$, $t \in [t(0), t(N)]$ can simply be enforced through constraints on the state at event instants only

$$\underline{h} \leq Hx(k) \leq \bar{h}, \quad k \in \mathbb{Z}_{[0, N]}. \quad (23)$$

Similarly, input bounds $\underline{u} \leq u_c(t) \leq \bar{u}$, $t \in [t(0), t(N))$ can be rewritten immediately as the linear constraints

$$\underline{u}q(k) \leq v(k) \leq \bar{u}q(k), \quad k \in \mathbb{Z}_{[0, N-1]}. \quad (24)$$

Different input bounds for different modes can be enforced by the logical constraint $[i(k) = \bar{i}] \rightarrow [\underline{u}_{\bar{i}}q(k) \leq v(k) \leq \bar{u}_{\bar{i}}q(k)]$, where $\underline{u}_{\bar{i}}$ and $\bar{u}_{\bar{i}}$ are upper and lower bounds of the input while in mode \bar{i} . Note that, differently from the standard discrete-time optimal control problem where constraint satisfaction is guaranteed only *pointwise in time*, in the event-driven approach state constraints are enforced *continuously on time*.

Additional operating constraints may be imposed on time intervals between two consecutive events

$$\underline{q} \leq q(k) \leq \bar{q}, \quad k \in \mathbb{Z}_{[1, N-1]}. \quad (25)$$

A finite \bar{q} imposes a maximum time for each control action, in order to prevent the system from running in open loop for too long until the next event. A minimum duration \underline{q} ensures a minimum time interval between two events (and thus between two mode switches), therefore avoiding undesirable effects such as high frequency chattering and control-induced Zeno behaviors [3]. More in detail, if constraint (25) is enforced, no solution that chatters with period smaller than \underline{q} is generated by the control strategy. Constraint softening may be used to avoid infeasibility when chattering cannot be avoided, thus resulting in the largest possible chattering period. Furthermore, (25) ensures that the time-length of the optimization problem is at least $N\underline{q}$. Finally, the lower bound \underline{q} can be used to account for the computation time of the optimal control problem (16). The minimum dwell time may be used there to guarantee that there is enough time to update the control input before the next event occurs.

Constraints on event instants $\underline{t}_k \leq t(k) \leq \bar{t}_k$, $k \in \mathbb{Z}_{[1, N]}$ can also easily be enforced, since time is a state variable on the optimization problem (16). These may be combined with state constraints to enforce that at a time instant during a given interval, the state value is within a given range.

3.3 Numerical Example

Consider the well-known “train–gate” benchmark for hybrid systems [17], commonly used for verification purposes, slightly modified and proposed here as a control problem.

The system is composed of a train and a gate. The control objective is to let the train cross the gate as fast as possible in a safe condition, i.e., the gate must be closed when the train crosses it. The well known linear hybrid automaton describing the system model is shown in Figure 2. The discrete state of the system is composed of the discrete state of the train and of the gate, whose dynamics are described by the automata in Figure 2. The train can be in an *arriving (Ar)*, *crossing (Cr)*, *leaving (L)*, or *far (F)* situation, depending on its position, the gate can be *open (O)*, *closing (Cl)*, *closed (C)* or *idle (I)*.

The continuous states of the system are the train position x^1 and the gate opening percentage x^2 , where $x^2 = 0$ means completely closed while $x^2 = 1$ means completely open. Instead of by the differential inclusions [17] used for verification, we define the dynamics by $\dot{x} = u(t) + f_i$, where $f_i(t) = \begin{bmatrix} f^1(t) \\ 0 \end{bmatrix}$, $u(t) = \begin{bmatrix} u^1(t) \\ u^2(t) \end{bmatrix}$ and $\underline{u}_i^j \leq u^j \leq \bar{u}_i^j$, $j = 1, 2$, and i is the system mode. The system modes are the cartesian product of the states of the train and the gate automata, hence 16 in total. The numerical values can be found in [9, Sec. 5.2.3].

Consider the following problem: from the initial state $\begin{bmatrix} x_{0c} \\ x_{0b} \end{bmatrix}$ with $x_{0c} = \begin{bmatrix} -20 \\ 1 \end{bmatrix}$ and $x_{0b} = (Ar, Cl)$, the train must safely cross the gate in minimum time. The minimum time criterion (19) where the target state was $\hat{x} = \begin{bmatrix} 40.3 \\ 1 \\ (F, I) \end{bmatrix}$ was applied with $N = 5$, under the safety constraint imposing that the discrete state (Cr, O) is never reached.

For control purposes we have modelled the system as a icHA (1)–(6). Figure 3 shows the regions of the continuous-state space corresponding to the modes of the train–gate system, and the optimal trajectory generated by the event-driven approach for the above stated problem plotted as a solid line. The x^1 axis is partitioned in four intervals, representing the train modes *Ar*, *Cr*, *L*, and *F*, and the x^2 axis, relative to the gate, in two intervals representing *Cl* (and *O*), and *C*.

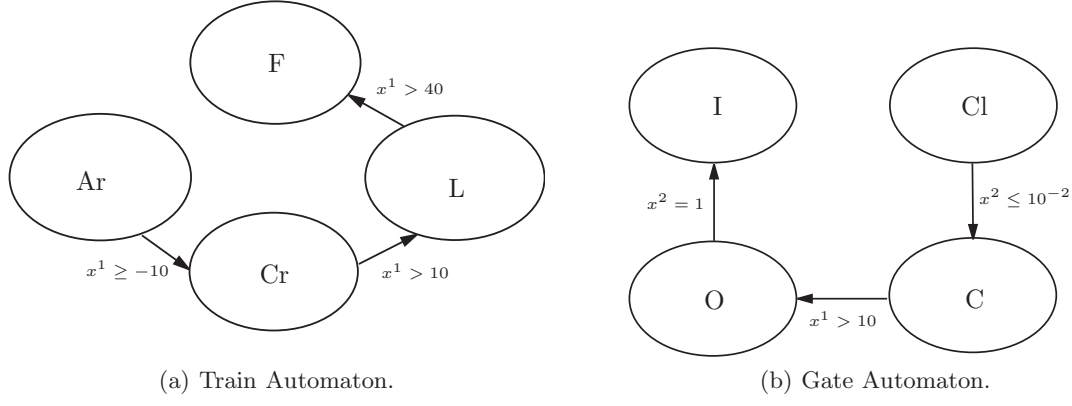


Fig. 2. Automata that describe the Train-Gate system.

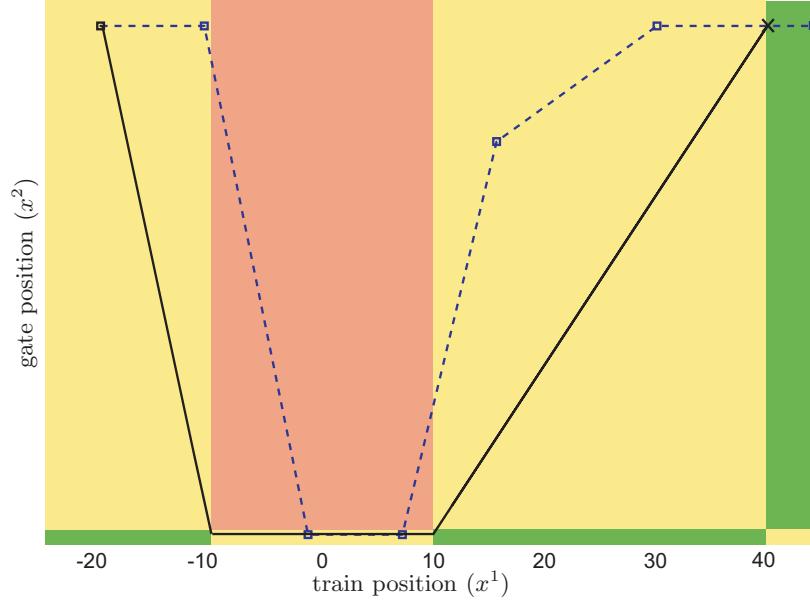


Fig. 3. Train-gate trajectory with minimum time control. The trajectory obtained by event-driven control is shown as a solid line, the trajectory obtained by discrete-time control ($N = 6$) is shown as a dashed line.

The target state \hat{x} is reached in 93.8 time units, with a trajectory that does not cross the unsafe region ($\{x \in \mathbb{R}^2 : 10 \leq x^1 \leq 10, 10^{-2} \leq x^2 \leq 1\}$). The CPU-time to compute the optimal trajectory is 0.26 seconds².

N	T_s (t.u.)	T_{cpu} (s)	T_{viol} (t.u.)	$T_{viol}^{(sup)}$ (t.u.)
5	20.00	0.29	3.82	40.00
6	16.66	0.86	21.83	33.33
10	10.00	10.93	9.82	20.00
15	6.66	640.21	6.55	13.33
e.d.	—	0.26	0	0

Table 1

Numerical results of the time-discretization approach (e.d. = event-driven (5), t.u.= time units).

Table 1 reports the results of the event-driven control compared to a discrete-time solution of the same problem. The time horizon of the discrete-time approach is 100 time units. The minimum-time criterion, which cannot be

² All the simulations presented in this paper have been performed on a Pentium IV-M 2.0 GHz with 1 GByte RAM running Cplex 9.0 and Matlab 6.5.

perfectly enforced in a discrete-time approach, is replaced by minimizing the tracking error between the current and target states $(\hat{x}_c, \hat{x}_b) = (40.3, (F, I))$. In Table 1, N is the number of time steps, T_s is the sampling period, T_{cpu} is the computation time. The dashed line in Figure 3 shows the trajectory obtained by discrete time control with $N = 6$. The unsafe situation of a train crossing the open gate is effectively attained during the intersampling. This is not surprising, as in the discrete-time formulation the constraints are only enforced at sampling instants. In Table 1, T_{viol} indicates the time period during which the current discrete-time solution violates the safety constraint. $T_{viol}^{(sup)} = 2T_s$ is the upper bound on T_{viol} , due to the fact that the safety constraints can be violated up to one sampling period when entering the gate and up to one sampling period when leaving from it. By decreasing T_s , also $T_{viol}^{(sup)}$ decreases, ensuring a better system safety. However, the number of required control steps increases for a fixed time-horizon, and hence the complexity of the optimization problem increases as shown in Table 1.

4 Event-Driven Model Predictive Control

The event-driven optimal control approach of Section 3 is an open-loop one. In this section we introduce an event-driven closed-loop strategy based on Model Predictive Control (MPC) concepts [10].

Given an icHA and its eMLD translation obtained as described in Section 2.1, consider again the optimal control problem (16). The event-driven Model Predictive Control (eMPC) strategy is defined as follows:

1. Let N be the event horizon; at a generic time t set $t_0 = t$, $x_0 = x(t)$ in (16).
2. Solve problem (16). Let $\mathbf{v}^*(x(t)) \triangleq [v_{x(t)}^*(0), \dots, v_{x(t)}^*(N-1)]$ be the sequence of optimal input integral values, $\mathbf{q}^*(x(t)) \triangleq [q_{x(t)}^*(0), \dots, q_{x(t)}^*(N-1)]$ be the sequence of input action durations, $\mathbf{x}^*(x(t)) \triangleq [x_{x(t)}^*(1), \dots, x_{x(t)}^*(N)]$ be the predicted state values at event instants, and $\mathbf{t}^*(x(t)) \triangleq [t_{x(t)}^*(1), \dots, t_{x(t)}^*(N)]$ be the corresponding time instants at which the events occur, computed from initial state $x(t)$ and initial time t .
3. Compute the input value $u_c(t) = \frac{v_{x(t),c}^*(0)}{q_{x(t)}^*(0)}$, and apply $u(t) = \begin{bmatrix} u_c(t) \\ v_{x(t),b}^*(0) \end{bmatrix}$ during the time interval $[t, t + q_{x(t)}^*(0)]$ to the icHA³.
4. Set $t_0 = t + q_{x(t)}^*(0)$, $x_0 = x(t + q_{x(t)}^*(0))$ in (16) and go to Step 2.

The actual state $x(t + q_{x(t)}^*(0))$ at the end of each control action may be different from the predicted one $x_{x(t)}^*(1)$ because of external disturbances and modelling errors. In fact, also the time instant at which the optimization problem is repeated may be different from the scheduled instant $t + q_{x(t)}^*(0)$. By the closed-loop nature of the eMPC approach, the current state (and time) are measured or estimated again and a new updated optimal input sequence is computed.

4.1 An Example of eMPC

Consider a system having two continuous states x^1 and x^2 , and two state thresholds $[\delta_{e_x}^1 = 1] \leftrightarrow [x^1 \leq 0]$, $[\delta_{e_x}^2 = 1] \leftrightarrow [x^2 \leq 0]$, so that the system has four modes. Each mode corresponds to an orthant of the Cartesian plane, where $i = 1$ corresponds to the positive orthant and the other orthants are numbered clockwise. The system has two inputs $-50 \leq u^1 \leq 50$ and $-50 \leq u^2 \leq 50$, and the vectors and matrices that define Equation (1) for $i = 1, \dots, 4$ are $f_1 = f_4 = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$, $f_2 = f_3 = \begin{bmatrix} -1 \\ 0 \end{bmatrix}$, $B_1 = \begin{bmatrix} 0 & 0 \\ 0 & 1.4 \end{bmatrix}$, $B_2 = \begin{bmatrix} 0 & 0 \\ 0 & 1.5 \end{bmatrix}$, $B_3 = \begin{bmatrix} 0 & 0 \\ 0 & 1.15 \end{bmatrix}$, $B_4 = \begin{bmatrix} 1 & 0 \\ 0 & 2.3 \end{bmatrix}$. Moreover, there are additional constraints on the inputs: when in mode $i = 1$ it must hold that $u^2 \geq -2$, $[i = 2] \rightarrow [u^2 \leq -0.5]$, $[i = 3] \rightarrow [u^2 \leq 2]$, $[i = 4] \rightarrow [u^1 \leq 2]$ and $[i = 4] \rightarrow [-0.5 \leq u^2 \leq 2]$.

We want to bring the state of the system from $x_0 = \begin{bmatrix} 0.1 \\ 2 \end{bmatrix}$ to $\hat{x} = \begin{bmatrix} -1 \\ 3 \end{bmatrix}$ while minimizing function (17) with norm $p = \infty$, $Q_1 = \begin{bmatrix} 10 & 0 \\ 0 & 10 \end{bmatrix}$, $Q_2 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$, $R_1 = \begin{bmatrix} 10^{-3} & 10^{-3} \end{bmatrix}$, $R_2 = 1$, and $0.1 \leq q \leq 50$. We have set $\hat{q} = 0.1$, $\hat{v} = u_\infty \hat{q}$, where $u_\infty = \begin{bmatrix} -1 \\ 0 \end{bmatrix}$. In order to test the robustness of the eMPC strategy with respect to disturbances, we assume that the system is perturbed by input-additive disturbances, so that the continuous state dynamics is

³ Different strategies may be proposed here, for example apply $u_c(t)$ during the interval $[t, t + \max\{q_{x(t)}^*(0), T_s\}]$, where T_s is a given minimum time interval (possibly covering more than one optimal event instants) to prevent out-of-time computation problems due to a small duration $q_{x(t)}^*(0)$.

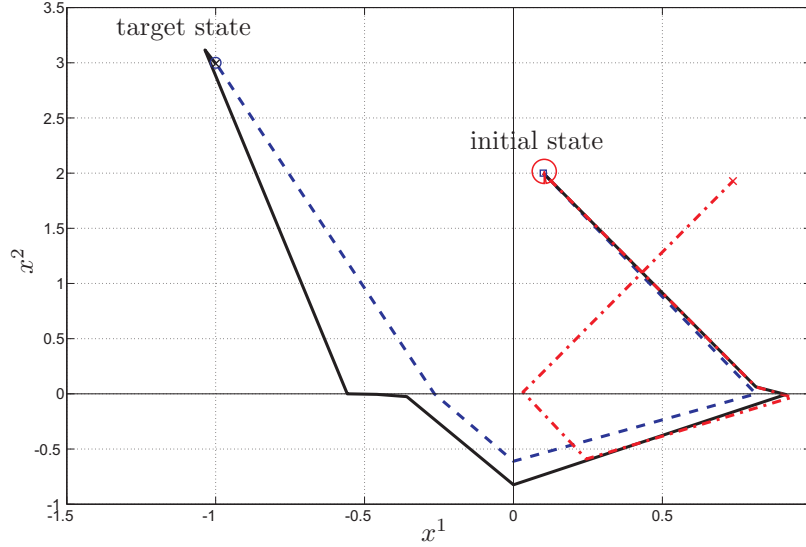


Fig. 4. Event-driven MPC example in the undisturbed (dashed) and disturbed (solid) cases, and comparison with the open-loop event-driven optimal control for the same disturbance realization (dash-dotted).

$\dot{x}(t) = B_{i(t(k))}(u(t(k)) + \nu(k)) + f_{i(t(k))}$, for all $t \in [t(k), t(k+1))$, where $\nu(k)$, $k \in \mathbb{Z}_{0+}$, is a sequence of time-uncorrelated stochastic vectors in which each component is independent from the other and uniformly distributed in $[-0.1, 0.1]$.

Figure 4 reports the continuous-time trajectories generated by the eMPC controller with a prediction horizon of 4 events, and reiterated for 8 consecutive steps. In the undisturbed case (dashed line) the closed-loop eMPC strategy trajectory coincides with the open-loop optimal one; four control actions, corresponding to four mode switches, are required to bring the system to the target state. In the presence of disturbances the eMPC (solid line) is able to counteract them, and to still bring the system close to \hat{x} , even if a larger number of control actions with respect to the undisturbed case is required. The trajectory obtained by the open-loop optimal policy under the effect of the same disturbance realization is plotted as a dash-dotted line, showing that the effects of the disturbance are not negligible, due to the switching nature of the system.

4.2 Conditions for Convergence of Closed-loop eMPC

In this section we prove closed-loop convergence properties of eMPC by resorting to classical techniques employed in nonlinear and hybrid MPC analysis [8, 25–27] and specializing them to the present continuous-time and event-driven context.

In the following analysis we consider the case of terminal equality constraint $\mathcal{X}_N = \{\hat{x}\}$ and $\mathcal{T}_N = \{\hat{t}\}$ or $\mathcal{T}_N = \mathbb{R}_{0+}$, while the case of terminal polyhedral set is discussed in [9, Sec. 5.4.2].

Definition 4.1 A state value $\bar{x} = \begin{bmatrix} \bar{x}_c \\ \bar{x}_b \end{bmatrix}$ is an equilibrium point for the icHA in mode \bar{i} if and only if there exists a steady state input value $\bar{u}_\infty = \begin{bmatrix} \bar{u}_{c,\infty} \\ \bar{u}_{b,\infty} \end{bmatrix}$ and $\bar{\delta}_{e,\infty}$ such that: (i), $B_{\bar{i}}\bar{u}_{c,\infty} + f_{\bar{i}} = 0$; (ii), $\bar{\delta}_{e,\infty} = f_{EG}(\bar{x}_c, \bar{u}_{c,\infty}, t)$, for all $t \geq 0$, where f_{EG} is the event generator (2); (iii), $\bar{x}_b = f_{aFSM}(\bar{x}_b, \bar{u}_{b,\infty}, \bar{\delta}_{e,\infty})$; (iv), $\bar{i} = [1 \dots s] \cdot f_{MS}(\bar{x}_b, \bar{u}_{b,\infty}, \bar{\delta}_{e,\infty})$.

Definition 4.1 requires that the input \bar{u}_∞ maintains the continuous state, the discrete state, and the mode constant. For instance the target state $\begin{bmatrix} -1 \\ 3 \end{bmatrix}$ in the example of Section 4.1 is an equilibrium point of mode $i = 4$ with steady-state input $\bar{u}_\infty = \begin{bmatrix} -1 \\ 0 \end{bmatrix}$.

4.2.1 Terminal Equality Constraints

When the terminal constraints $x(N) = \hat{x}$, $t(N) = \hat{t}$ are included, the terminal cost F is removed from (17). Let $\chi(k) \triangleq \begin{bmatrix} x(k) \\ t(k) \end{bmatrix}$ denote the full state of the eMLD system at a generic time $t(k)$. Let $J^*(\chi(k))$ be the optimal cost

of Problem (16), $\mathbf{X}^*(\chi(k)) = [\chi_{\chi(k)}^*(1), \dots, \chi_{\chi(k)}^*(N)]$ and $\mathbf{w}^*(\chi(k)) = [w_{\chi(k)}^*(0), \dots, w_{\chi(k)}^*(N-1)]$ be⁴ the optimal state and optimal input trajectories, respectively, where $w_{\chi(k)}^*(i) = \begin{bmatrix} v_{\chi(k)}^*(i) \\ q_{\chi(k)}^*(i) \end{bmatrix}$. For the sake of notation, denote by $\chi(k+1) = G(\chi(k), w(k))$ the state update function (15).

Theorem 4.1 *Let $\mathcal{X}_N = \{\hat{x}\}$, $\mathcal{T}_N = \{\hat{t}\}$, and let $\underline{q} = 0$. Let \hat{x} be an equilibrium point with corresponding steady-state input \hat{u} , let $\hat{q} = 0$, $\hat{v} = \begin{bmatrix} 0 \\ \hat{u}_b \end{bmatrix}$, and assume that $(\hat{x}, \hat{t}, \hat{q}, \hat{v})$ satisfies constraints (16c) and (16d). Let L be a function such that $L(\hat{x}, \hat{t}, \hat{q}, \hat{v}) = 0$ and $L(x, t, q, v) \geq \psi\left(\left\|\frac{x - \hat{x}}{t - \hat{t}}\right\|\right)$, where $\psi : \mathbb{R}_{0+} \rightarrow \mathbb{R}_{0+}$ is a nondecreasing function, $\psi(0) = 0$, $\psi(\alpha) \in \mathbb{R}_+$, for all $\alpha \in \mathbb{R}_+$. If Problem (16) is feasible for the initial state $x_0 = x(0)$ and $t_0 = 0$, then it is recursively feasible, i.e., it is feasible for all $\begin{bmatrix} x(k+1) \\ t(k+1) \end{bmatrix} = G(\chi(k), w_{\chi(k)}^*(0))$, $k \in \mathbb{R}_+$, and moreover $\lim_{t \rightarrow \hat{t}} x(t) = \hat{x}$.*

Proof. We first prove feasibility. Assume Problem (16) admits a solution at event step $k = 0$, $\chi(k) = \begin{bmatrix} x(0) \\ 0 \end{bmatrix}$. Let $\mathbf{w}^*(\chi(k))$ be the corresponding optimal input sequence, and let $\chi(k+1) = \chi_{\chi(k)}^*(1)$. Consider the input sequence

$$\tilde{\mathbf{w}}(\chi(k+1)) = \left[w_{\chi(k)}^*(1), \dots, w_{\chi(k)}^*(N-1), \begin{bmatrix} 0 \\ \hat{u}_b \end{bmatrix} \right].$$

Then, $\chi_{\chi(k+1)}(i) = \chi_{\chi(k)}(i+1)$, for $i \in \mathbb{Z}_{[0, N-1]}$, and

$$\chi_{\chi(k+1)}(N) = G\left(\chi_{\chi(k+1)}(N-1), \begin{bmatrix} 0 \\ \bar{u}_{b, \infty} \end{bmatrix}\right) = G\left(\chi_{\chi(k)}^*(N), \begin{bmatrix} 0 \\ \bar{u}_{b, \infty} \end{bmatrix}\right) = \chi_{\chi(k)}^*(N).$$

Thus the sequence $\tilde{\mathbf{w}}(\chi(k+1))$ satisfies the dynamical, operating, and terminal constraints in (16), so Problem (16) is solvable at time $k+1$. By induction, solvability at $k=0$ implies solvability at all event steps $k \in \mathbb{Z}_+$.

We now prove convergence. Because of optimality, $J^*(\chi(k+1)) \leq J(\chi(k+1), \tilde{\mathbf{w}}(\chi(k+1)))$, where

$$J(\chi(k), \tilde{\mathbf{w}}(\chi(k+1))) = J^*(\chi(k)) - L(x(k), t(k), v_{\chi(k)}^*(0), q_{\chi(k)}^*(0)), \quad (26)$$

and hence $J^*(\chi(k+1)) \leq J^*(\chi(k))$. Since $J(\chi(k))$ is lower bounded by 0 and is not increasing with k , there exists $\lim_{k \rightarrow \infty} J(\chi(k)) = J_\infty$, so that $\lim_{k \rightarrow \infty} J(\chi(k+1)) - J(\chi(k)) = 0$, and hence $\lim_{k \rightarrow \infty} L(x(k), t(k), v(k), q(k)) = 0$. The last implies $\lim_{k \rightarrow \infty} \psi(\|\chi(k) - \hat{\chi}\|) = 0$, where $\hat{\chi} = \begin{bmatrix} \hat{x} \\ \hat{t} \end{bmatrix}$. Assume by contradiction $\|\chi(k) - \hat{\chi}\| \not\rightarrow 0$. Then there exists $\epsilon \in \mathbb{R}_+$ such that for all $k \in \mathbb{Z}_{0+}$ there exists $k \geq \bar{k}$ such that $\|\chi(k) - \hat{\chi}\| \geq \epsilon$. As ψ is nondecreasing, $\psi(\|\chi(k) - \hat{\chi}\|) \geq \psi(\epsilon)$, which contradicts $\lim_{k \rightarrow \infty} \psi(\|\chi(k) - \hat{\chi}\|) = 0$. Therefore, $\lim_{k \rightarrow \infty} \left\| \frac{x(k) - \hat{x}}{t(k) - \hat{t}} \right\| = 0$ and hence $\lim_{k \rightarrow \infty} x(k) = \hat{x}$, $\lim_{k \rightarrow \infty} t(k) = \hat{t}$. By linearity of $x(t)$ between two consecutive events it also follows that $\lim_{t \rightarrow \hat{t}} x(t) = \hat{x}$. \square

Note that function ψ is also called a function of class \mathcal{M} in [27]. The condition of ψ being of class \mathcal{M} was sufficient in the proof of Theorem 4.1 to ensure convergence of $\|\chi(k) - \hat{\chi}\|$ to zero when $\psi(\|\chi(k) - \hat{\chi}\|)$ converges to zero, a property which is directly assumed in [26]. Note also that the assumption about the existence of function ψ is satisfied when L is strictly convex with respect to x and t .

The trajectory obtained by the approach of Theorem 4.1 is defined for $t \in [0, \hat{t}]$. For $t \geq \hat{t}$ the target state can be maintained by applying a steady state input, if this exists accordingly to Definition 4.1. Despite convergence of x is ensured in finite time \hat{t} , it may be asymptotic with respect to the number k of events.

Next Theorem 4.2 considers the case in which the terminal time $t(N)$ is unconstrained (i.e., $\mathcal{T}_N = \mathbb{R}_{0+}$), L does not depend on t (for instance, $Q_2 = 0$ in (18)), and in which $\underline{q} > 0$. The lower bound $\underline{q} > 0$ ensures a minimum dwell time of the system between two consecutive mode switches, which may prevent for instance that $q(k)$ gets too small for solving the next optimization problem.

Theorem 4.2 *Let $\mathcal{X}_N = \{\hat{x}\}$, $\mathcal{T}_N = \mathbb{R}_{0+}$ and let $\underline{q} > 0$. Let \hat{x} be an equilibrium point with corresponding steady-state input \hat{u} , and assume there exists \hat{q} , $\underline{q} \leq \hat{q} \leq \bar{q}$, such that $(\hat{x}, \hat{t}, \hat{q}, \hat{v})$ satisfies constraints (16c) and (16d) for $\hat{v} = \begin{bmatrix} \hat{q} \\ \hat{u}_b \end{bmatrix}$*

⁴ When using the full state χ we use the notation $\chi(k)$ for $\chi(t(k))$, as stated in Section 1.1.

and for all $\hat{t} \geq 0$. Let L be independent of t , be such that $L(\hat{x}, t, \hat{q}, \hat{v}) = 0$, for all $t \in \mathbb{R}$, and $L(x, t, q, v) \geq \psi(\|x - \hat{x}\|)$, where $\psi : \mathbb{R}_{0+} \rightarrow \mathbb{R}_{0+}$ is a nondecreasing function, $\psi(0) = 0$, $\psi(\alpha) \in \mathbb{R}_+$, for all $\alpha \in \mathbb{R}_+$. If Problem (16) is feasible for the initial state for $x_0 = x(0)$ and $t_0 = 0$, then it is recursively feasible, i.e., it is feasible for all $\begin{bmatrix} x(k+1) \\ t(k+1) \end{bmatrix} = G(\chi(k), w_{\chi(k)}^*(0))$, $k \geq 0$, and $\lim_{t \rightarrow \infty} x(t) = \hat{x}$.

Proof. The proof is similar to the proof of Theorem 4.1. Assume Problem (16) admits a solution at event step $k = 0$, $\chi(k) = \begin{bmatrix} x(0) \\ 0 \end{bmatrix}$. Let $\mathbf{w}^*(\chi(k))$ be the corresponding optimal input sequence, and let $\chi(k+1) = \chi_{\chi(k)}^*(1)$. Then, the shifted sequence

$$\tilde{\mathbf{w}}(\chi(k+1)) = \left[w_{\chi(k)}^*(1), \dots, w_{\chi(k)}^*(N-1), \begin{bmatrix} \hat{v} \\ \hat{q} \end{bmatrix} \right]$$

is feasible, because $(\hat{x}, \hat{t}, \hat{q}, \hat{v})$ is an equilibrium quadruple which satisfies constraints (16c) and (16d), for all $\hat{t} \geq 0$, and hence

$$x_{\chi(k+1)}^*(N) = x_{\chi(k+1)}^*(N-1) = x_{\chi(k)}^*(N).$$

Therefore, (26) still holds and hence $\lim_{k \rightarrow \infty} L(x(k), t(k), v(k), q(k)) = 0$. The latter implies that $\lim_{k \rightarrow \infty} \psi(\|x(k) - \hat{x}\|) = 0$ and, as shown in the proof of Theorem 4.1, that $\lim_{k \rightarrow \infty} x(k) = \hat{x}$. Since $t(k+1) - t(k) = q(k) \geq \underline{q} > 0$, $\lim_{k \rightarrow \infty} t(k) = +\infty$. Hence, $x(t)$ is defined for all $t \in \mathbb{R}_{0+}$ and by linearity of $x(t)$ between two consecutive events it follows that $\lim_{t \rightarrow \infty} x(t) = \hat{x}$. \square

In order to have that $\lim_{k \rightarrow \infty} v(k) = \hat{v}$, $\lim_{k \rightarrow \infty} q(k) = \hat{q}$, it is enough to assume that $L(x, t, q, v) \geq \psi \left(\begin{bmatrix} \|x - \hat{x}\| \\ \|v - \hat{v}\| \\ \|q - \hat{q}\| \end{bmatrix} \right)$.

Note that the eMPC controller designed in Section 4.1 satisfies the hypotheses of Theorem 4.2.

5 Conclusions

In this paper we have introduced integral continuous-time hybrid automata (icHA), a special class of continuous-time hybrid dynamical models that can be suitably controlled through numerically viable optimization tools. The key idea for reformulating the infinite-dimensional optimization problem into a tractable finite-dimensional one is to use an event-driven control strategy. Differently from standard optimization-based discrete-time techniques, the event-driven approach guarantees that the constraints are enforced continuously in time, while keeping the computation load comparable. This paper only scratched the surface of the modelling power of the approach, by emphasizing for instance the relations that exist between icHA and linear hybrid automata. Finally, we have shown how closed-loop control strategies for icHA can be designed through receding horizon ideas, for which we have provided sufficient conditions for finite time and asymptotic convergence.

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